

Induced earthquakes in the development of unconventional energy resources

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Abstract It has long been known that human activities such as waste fluid disposal and reservoir impoundment may cause earthquakes. Recently, anthropogenic activities to tackle the increasing energy demand and to address climate change issues are also reported to induce earthquakes. These activities have a common attribute in that fluids are injected and extracted underground and induce spatiotemporal changes of pore pressure and stress, which may cause slip on faults. Induced earthquakes not only pose significant impacts on seismic hazard assessment and preparation, but also raise the question to the society as how to balance the economic needs of resources development and the public's concerns about potential environmental impacts. Here we review the observations of fluid-injection/extraction induced earthquakes, ground deformation associated with these activities, and their physical mechanisms. Furthermore, we discuss the influences of induced earthquakes on seismic hazard models, regulatory policies on these anthropogenic activities, and current development of academic, industrial and government initiatives and collaborations in order to understand this intriguing phenomenon and address associated challenges.

Keywords Induced earthquake, Fluid injection, Energy demand, Climate change

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1. Introduction

Earthquakes are a major threat to the human society, as vividly demonstrated by the recent 2011 M_w 9.0 Tohoku-oki (Japan), 2015 M_w 8.3 Illapel (Chile), and 2015 M_w 7.8 Gorkha (Nepal) earthquakes (e.g., Yue and Lay, 2011; Yang et al., 2015; Yin et al., 2016, 2017). Accordingly a major challenge in hazard mitigation is the fundamental understanding of earthquake physics, so that appropriate societal responses can be formulated for mitigating major seismic risk to human lives and infrastructure. In addition to tectonic earthquakes, it has long been known that human activities such as water

reservoir impoundment and waste fluid disposal may cause earthquakes, termed induced earthquakes (e.g. McGarr et al., 2002). Consequently there have been relevant review papers to discuss this intriguing phenomenon, mostly focusing on the overview of case studies of well documented induced earthquakes. For instance, Nicholson and Wesson (1992) summarized the earthquakes triggered by deep well activities, including deep well fluid injection and massive fluid extraction. Talwani (1997) documented reservoir-induced earthquakes and discussed two categories of seismicity by their occurrence time relative to the initial impoundment. McGarr et al. (2002) reviewed case histories of anthropogenic seismicity, including mining, quarry, fluid injection, large impounded reservoirs, as well as hydrocarbon reservoir

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compaction.

In recent decades, there is also heightened concern of a further complication, in that anthropogenic activities tackling climate change and energy demand (e.g. hydraulic fracturing for shale gas exploration, large-volume wastewater disposal, natural gas storage and extraction cycles) can induce seismicity and trigger relatively large quakes. After assembling 70 cases of hydrocarbon fields for which a connection between unusual seismicity patterns and hydrocarbon production had been suggested, Suckale (2009) found a striking feature that occurrences of induced earthquakes had a distinct regional character. Ellsworth (2013) reviewed the increase in seismic activity that may be primarily related with fluid injection into deep wells to dispose wastewater partly produced in hydraulic fracturing in central and eastern United States. Mostly recently, Grigoli et al. (2017) presented a summary of observations and outstanding questions in the monitoring, discrimination and management of earthquakes induced by various anthropogenic sources in Europe.

Even though there is a clear link between induced earthquakes and anthropogenic activities, many critical questions regarding this intriguing phenomenon remain unanswered. Consequently controversy has emerged regarding whether certain cases of seismicity had been indeed triggered by human activities. For instance, in Barnett Shale and Cogdell, Texas, the question was raised whether extensive development of unconventional gas resources has resulted in injection-induced earthquakes (Frohlich, 2012; Gan and Frohlich, 2013). In this paper, we do not attempt to provide an exhaustive review of all types of induced earthquakes. Rather of being region specific as in several recently published review articles, we categorize the induced seismicity observations by their potential triggering sources and focus the discussion on their physical mechanisms, hazard and regulatory policy implications. In addition to seismological observations, which constitutes the bulk of data available up to date for induced earthquakes, we also discuss other types of observations (e.g., geodetic surveys) and approaches (e.g., statistics analysis, numerical modeling) that can contribute to our understanding of the source processes. We acknowledge that the study of induced earthquakes is evolving so rapidly that some parts of this review may soon be outdated. Nevertheless, given the dramatic increase in numbers of earthquakes related to unconventional energy resources exploration in the past decade, this article aims to serve as a timely introduction to current issues in induced seismicity of interest to seismologists and the general public.

2. Seismic and geodetic observations

In view of the long history of induced seismicity documented in previous reviews (e.g. Nicholson and Wesson, 1992; McGarr et al., 2002; Ellsworth, 2013), this article focuses on

more recent anthropogenic activities to tackle energy demand and climate change, specifically, earthquakes potentially induced by (1) hydraulic fracturing (fracking), (2) waste water disposal, (3) geothermal energy extraction, (4) CO₂ sequestration, and (5) cyclic injection/extraction of natural gas (Figure 1). In this section, we introduce seismological and geodetic observations of earthquake activity and ground deformation associated with the above five scenarios.

2.1 Observed induced seismicity

It is well known that induced seismicity can be caused by the injection of waste fluid into disposal wells. A textbook example is the series of large earthquakes in the Denver area in the 1960s, due to hazardous waste injection at Rocky Mountain Arsenal in Colorado (Evans, 1966; Healy et al., 1968). In the 1970s an interdisciplinary study was undertaken in this site, synthesizing comprehensive investigations in seismology, hydrogeology and rock physics. This integrated effort has contributed to seminal advances in our understanding of the mechanics of induced seismicity (Raleigh et al., 1976). More recently, significant seismicity likely related to the disposal of wastewater in wells has been widely observed, especially in large areas long considered to be geologically stable (e.g. Petersen et al., 2016). Some of the earthquakes caused by the disposal of fluids are relatively strong and widely felt at large distances. For instance, two moderate-sized earthquakes (M_w 5.7 in 2011 and M_w 5.8 in 2016) in Oklahoma likely related to large volume wastewater disposal in nearby wells were felt in at least 17 states and caused damage in the epicentral region (Keranen et al., 2014; McGarr et al., 2015; Yeck et al., 2017).

Compared to wastewater disposal, hydraulic fracturing (fracking), an innovative technique to stimulate fracture growth and increase permeability so as to extract gas from the low-permeability shale formation, had been thought to induce typically small earthquakes with magnitude less than M_w 1. However, a few recent cases have shown that magnitudes of earthquakes related to fracking may exceed M_w 4 (British Columbia Oil and Gas Commission, 2012; Ellsworth, 2013; Atkinson et al., 2016). As shown in Figure 2, Fox Creek in Alberta, Canada, used to be a seismically quiescent area before the hydraulic fracturing operation started in March 2010. Seismicity has dramatically increased since December 2013 when fracking induced earthquakes were first reported in this area (Schultz et al., 2017).

Earthquakes have also been reported to associate with the exploitation of geothermal resources, in which water is pumped into and out of a reservoir (e.g. Häring et al., 2008; Goertz-Allmann et al., 2011; Brodsky and Lajoie, 2013). In the Salton Sea Geothermal Field, USA, long-term evolution of seismicity appears to be modulated by the net fluid volume (the difference between extraction and injection) (Brodsky

and Lajoie, 2013). Extensive microseismicity was detected during the fracturing process at the European Geothermal Hot Dry Rock research site at Soultz-sous-Forêts, France, where hydraulic stimulation is applied to enhance reservoir permeability and heat exchange efficiency. The largest events of M_L 2.7 to M_L 2.9 occurred during the shut-in period (Michelet and Toksöz, 2007). The Enhanced Geothermal System (EGS) project in Basel, Switzerland, is arguably the most notable example of earthquakes directly related to hydraulic stimulation in the process of exploiting geothermal resources. Earthquakes of M_L 2.6 and M_L 3.4 were induced during the peak injection and after well shut-in, respectively, which caused damages to local residences (Giardini, 2009). Public concern over induced seismicity eventually led to the definitive suspension of the Basel EGS project.

The fourth scenario is in connection with underground storage of natural gas, adopted worldwide to meet seasonal variations in demand, which requires cyclic injection and extraction of natural gas underground (e.g. Priolo et al., 2015). For instance, near the Hutubi gas reservoir in Xinjiang, the largest underground repository for natural gas in China, a sequence of earthquakes occurred soon after the injection was initiated in 2013, with the largest magnitude of M_L 3.5 (Figure 3).

The fifth scenario is to capture and sequestration of CO₂ in deep geological formations, proposed as an option to mitigate global warming due to anthropogenic emission of greenhouse gases. It has been suggested that this could result in reduction in CO₂ emissions over the century that is comparable to that expected from efficiency improvements and large-scale deployment of renewable energy resources (IPCC, 2005). How-

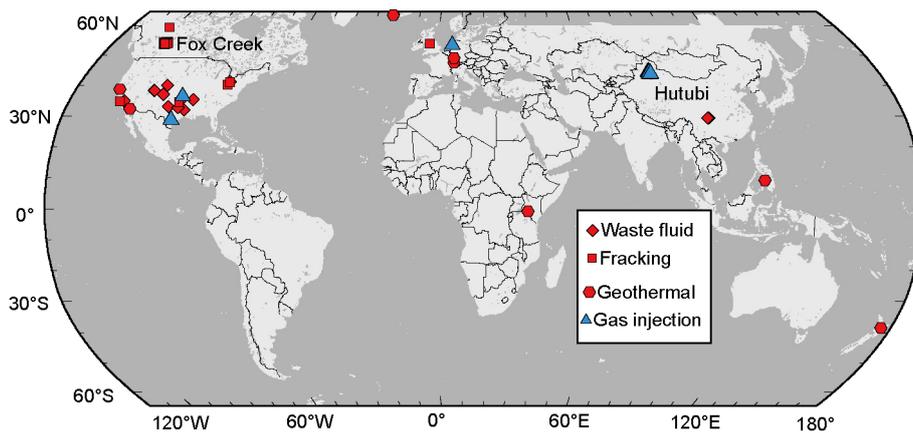


Figure 1 A global map showing reported induced earthquakes. Fox Creek, Alberta, Canada and Hutubi, Xinjiang, China are marked where local seismicity is shown in Figures 2 and 3, respectively.

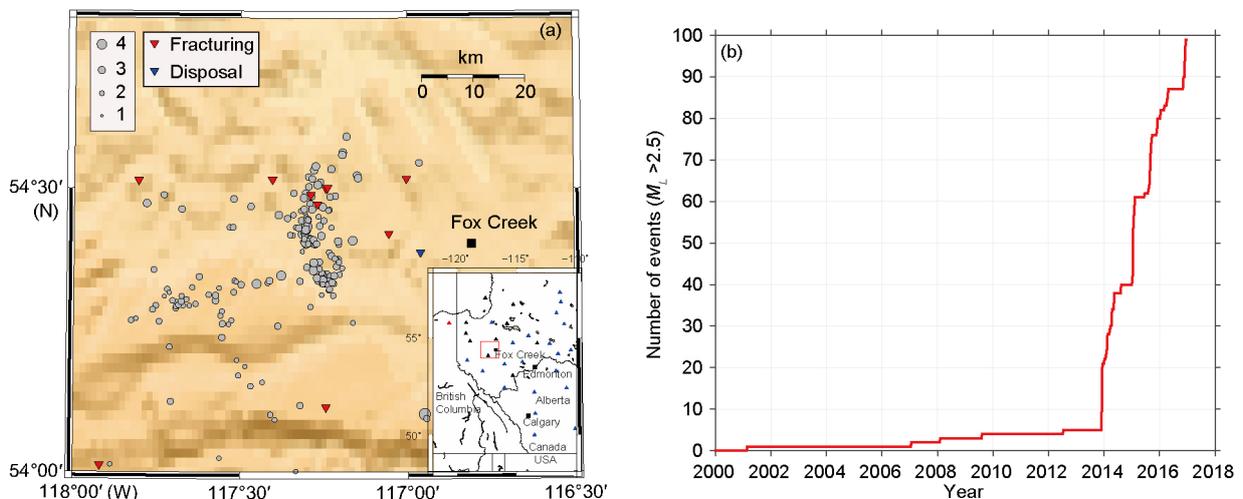


Figure 2 Seismicity near Fox Creek, Alberta, Canada. (a) Earthquake epicenters from the Canadian National Seismograph Network (CNSN), 2005–2016. There were no CNSN cataloged events in this area 1985–2005. Inverted triangles show the locations of hydraulic fracturing (red) and waste water disposal (blue) wells that have been identified being associated with $M > 3$ earthquakes in the study by Atkinson et al. (2016). Inset shows the location of Fox Creek area, and regional seismic stations (triangles, blue: CRANE, black: Raven, red: CNSN). (b) Cumulative number of earthquakes with $M_L > 2.5$ (excluding blast events) within 100 km radius from Crooked Lake (54.45°N, 117.25°W). Hydraulic fracturing started in March 2010 in this area, with the first induced earthquake reported in December 2013.

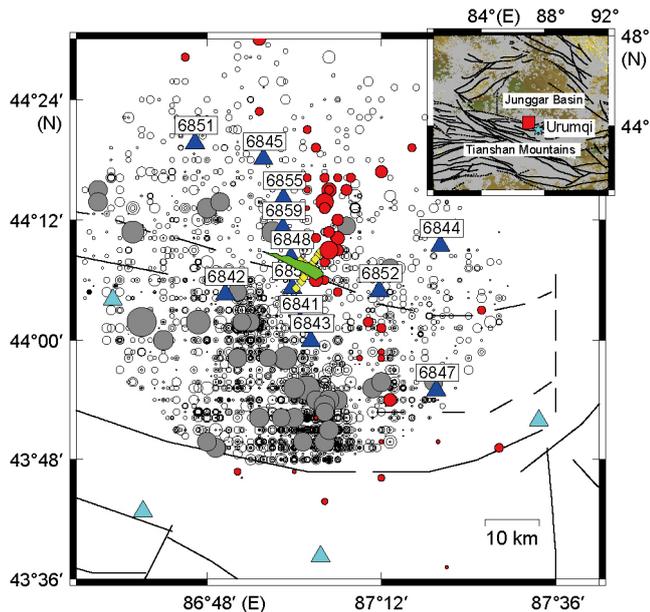


Figure 3 Map showing faults (lines), seismicity (circles), and seismic (triangles) and GPS (yellow diamonds) stations in the vicinity of the Hutubi gas repository (HGR) (green area). Grey dots denote the earthquakes with magnitudes larger than 3 since 1970. Red dots represent earthquakes occurred from June to August, 2013. Blue triangles are newly deployed seismic stations in 2013. Cyan triangles denote permanent stations operated by the Xinjiang Earthquake Administration. Zoom-in map showing location of the HGR (red square), faults (lines), and seismicity (grey dots) in Xinjiang.

ever, serious concerns were raised on the risk of induced seismicity, especially in the confining units for a geologic repository of supercritical CO₂ (Zoback and Gorelick, 2012). In a recent study, Gan and Frohlich (2013) reported an instance where the injection of CO₂ has triggered earthquakes with magnitudes 3 and larger in the Cogdell oil field, Texas.

2.2 Ground deformation associated with fluid injection

Human activities can cause ground deformation. Examples include coal mining (Carnec et al., 1996; Haynes et al., 1997), extracting petroleum and gas (Massonnet et al., 1997; Fielding et al., 1998), extracting groundwater (Galloway et al., 1998; Amelung et al., 1999), and geothermal fluid production (Barbour et al., 2016). Geodetic methods, especially GPS and InSAR (Interferometric Synthetic Aperture Radar) have been widely used to measure the scale, magnitude, and rate of the ground deformation (Massonnet and Feigl, 1998; Rosen et al., 2000; Bürgmann et al., 2000).

The wastewater disposal and injection of gas can potentially create some measurable surface deformation, due to either the expansion of the reservoir caused by the extra fluid or the induced fault slip, including aseismic slip and earthquakes. For instance, wastewater injection has caused vertical uplift, which was measured by InSAR images near several disposal wells in eastern Texas (Shirzaei et al., 2016). The large injection volume (7×10^5 – 9×10^5 m³/year) and

the long operation period (2005–2007) may be the major factors for causing the line-of-sight (LOS) uplift rate up to 3 mm/year. Based on local geological profiles and hydraulic properties, the pore pressure increase due to injection is estimated to be around 0.5 to 1.5 MPa at the hypocentral depth of the 2012 M_w 4.8 earthquake (Shirzaei et al., 2016), the largest among a sequence of seismicity between two closely spaced disposal wells and ~20 km from the area of largest uplift rate inferred from InSAR observations. In another example, InSAR measurements show surface uplift and subsidence in heavy oil fields in Alberta, Canada, and the deformation is highly correlated with the stimulation and extraction phases of cyclic steam operation (Granda et al., 2012; Samsonov S, private communication). InSAR images also detected ground deformation at a CO₂ sequestration site in southeast Saskatchewan, Canada (Samsonov et al., 2015).

However, at several locations of gas injection in Australia, Algeria, and Utah, USA, InSAR measurements have shown surface uplift of several cm, but in each case no earthquakes larger than magnitude of zero have been recorded (Gan and Frohlich, 2013). Whether the difference stems from the gas and liquid injection remains unknown. Another case is from the Hutubi natural gas repository in Xinjiang, China, where earthquakes occur immediately after the gas injection. Measurements of campaign GPS show ground deformation, but other factors such as underground water extraction and seasonal variation pose significant challenge to pinpoint the contribution from gas injection to the surface deformation (Wang D et al., 2016).

Surface deformation directly caused by induced earthquakes has been reported for the 2011 M_w 5.3 Trinidad earthquake in Colorado (Barnhart et al., 2014), the 2016 M_w 5.8 Pawnee earthquake in Oklahoma (Yeck et al., 2017; Fielding et al., 2017; Grandin et al., 2017; Pollitz et al., 2017), and the 2016 M_w 5.0 Cushing earthquake in Oklahoma (Barnhart and Yeck, 2017). For the 2011 Trinidad earthquake, line-of-sight deformation over 6 cm was observed in InSAR data from the European Space Agency (ESA)'s Envisat satellite. Geodetic inversion suggests that the earthquake ruptured an 8–10 km long segment of a normal fault at depths of 1.5–6.0 km within the crystalline Precambrian basement underlying the Raton Basin sedimentary rocks (Barnhart et al., 2014). For the 2016 Pawnee earthquake, a region of line-of-sight shortening about 3 cm adjacent to the Pawnee main shock without surface rupture was shown in InSAR data from ESA's Sentinel-1A and -1B C-band radars and Canadian Radarsat-2 satellite. The general pattern of deformation is consistent with a shallow blind left-lateral strike-slip earthquake. The depth of maximum slip varies between slip models at 5.6, 7, and 12 km in Pollitz et al. (2017), Grandin et al. (2017), and Fielding et al. (2017), respectively. The variation might reflect the non-uniqueness in geodetic inversion and different choices of smoothing.

For the 2016 Cushing earthquake, the deformation signal is even clearer than that of the Pawnee earthquake, likely due to the shallow hypocentral depth and low atmospheric noise of InSAR data (Barnhart and Yeck, 2017). In contrast, there was no report of deformation observation for the 2011 M_w 5.7 Prague earthquake (Keranan et al., 2014) or the 2016 M_w 5.1 Fairview in Oklahoma (Barnhart et al., 2017). The lack of observed deformation for the 2011 Prague earthquake is surprising because the magnitude is similar to the Pawnee earthquake and its focal depth of 3.1 km (Summy et al., 2014) is even shallower than the 4.7 km depth of the Pawnee earthquake (Yeck et al., 2017). The lack of deformation observation of the Prague earthquake is probably due to the small number of available InSAR satellite in the orbit and small number of acquired data around 2011. We expect to see more reports on deformation caused by the triggered earthquakes around the world considering the wide-spreading practice of hydraulic fracturing and wastewater disposal.

3. Mechanism of induced earthquakes

3.1 Fluid diffusion and poroelasticity

Earthquake triggering due to external stress perturbations are commonly explained using the Coulomb failure criterion (Harris, 1998; Steacy et al., 2005), where the Coulomb Failure Stress change is defined as

$$\Delta\text{CFS} = \Delta\tau - \mu\Delta(\sigma - p), \quad (1)$$

here $\Delta\tau$ and $\Delta\sigma$ are shear (positive in slip direction) and normal (positive in compression) stress changes, respectively, resolved onto a certain fault orientation; Δp is the pore pressure change, and μ is the dry friction coefficient on the fault, which usually ranges from 0.6 to 0.8. The difference between normal stress and pore pressure is defined as the effective normal stress $\Delta\bar{\sigma} = \Delta(\sigma - p)$. A positive Coulomb stress change ($\Delta\text{CFS} > 0$) promotes fault failure whereas a negative ΔCFS prohibits failure.

Figure 4 illustrates two plausible ways that fluid injection may affect the Coulomb stress and promote failure. First, fluid injection can lead to pore fluid diffusion along newly created fractures and/or pre-existing fault zones, temporally increase pore pressure hence reduce the effective normal stress, and bring a pre-existing fault or intact rock close to failure. It has long been postulated as a leading mechanism for earthquakes induced by oil and gas extractions (e.g., Hubbert and Rubey, 1959; Healy et al., 1968; Raleigh et al., 1976). Seismicity directly induced by pore pressure increase has been documented for both hydraulic fracturing and wastewater disposal scenarios. For example, seismic swarm activity has been reported during the hydraulic fracturing from a vertical borehole in the Barnett Shale formation

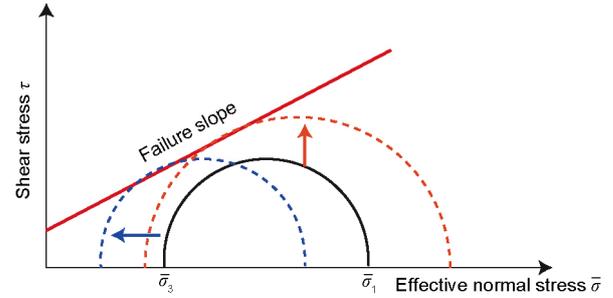


Figure 4 Two possible mechanisms fluid injection may induce earthquakes. Mohr Circle representations of stress state before perturbation (black, solid), after homogeneous pore pressure increase (effective normal stress decrease) (blue, dashed), and after solid matrix stress (shear and/or normal) changes (orange, dashed). Cohesion and friction coefficient are assumed to be constant before and after perturbation.

of the Fort Worth Basin (Fisher et al., 2004) as a result of fast fluid diffusion due to enhanced formation permeability (Shapiro and Dinske, 2009). In Oklahoma, fluid migration from high-rate disposal wells may be responsible for the rapid increase in seismicity in Oklahoma, and suggested regular reservoir pressure monitoring as means of hazard assessment (Keranan et al., 2014).

Second, fluid injection can directly perturb the solid matrix stresses (shear and normal) in the surrounding media and bring faults with preferred orientations closer to failure. This scenario does not necessarily require an increase in pore pressure, and may be particularly effective under hydraulic fracturing operations and extraction of fluids (Rudnicki, 1986; Segall, 1989; Segall and Lu, 2015; Deng et al., 2016; Chang and Segall, 2016). While wastewater disposal can last for years to decades, each stage of hydraulic fracturing typically lasts for a few hours, and each horizontal well is completed within a couple of weeks. Thus, the direct pore pressure increase may not be as significant on such short time scales, due to the low permeability of the shale formation. Recent studies of induced earthquakes in the western Canada sedimentary basin (WCSB) have found that most recent cases of induced earthquakes (2010-2015) of $M > 3$ are highly correlated in space and time with hydraulic fracturing, in contrast to deep disposal of coproduced wastewater for induced seismicity in the central US (Schultz et al., 2015; Atkinson et al., 2016; Bao and Eaton, 2016; Schultz et al., 2017). Although the differences in the total injection volume in disposal wells (sometimes up to 100 times) can play a role (Schultz et al., 2014; Mahani et al., 2017), the distinction between instantaneous solid matrix stress changes that are most effective during and shortly after hydraulic fracturing treatment and long-term pore pressure buildup from fluid diffusion may also be a key factor in the different correlations in central US and WCSB. To test this idea, Deng et al. (2016) developed a poroelasticity model for calculating the fully coupled solid matrix stress changes and fluid pressure diffusion in an anisotropic media due to multi-stage stimulation

and successfully explained the spatiotemporal distribution of an induced earthquake sequence in December 2013 near Fox Creek, Alberta, Canada. Their modeling results demonstrated that during the hydraulic fracturing the solid matrix stress changes on a pre-existing fault located 1–2 km from the horizontal well far exceed the pore pressure increase, and most of the seismicity in the December 2013 sequence is spatiotemporally correlated with the positive regime of the resulting Coulomb stress change. The poroelasticity model thus suggests, due to low permeability of shale formation, shear stress accumulation rather than diffusion of pore pressure is more likely the dominant factor bringing critically stressed medium to failure (Deng et al., 2016). Near-instantaneous stress redistribution caused by poroelastic coupling has also been suggested as the triggering mechanism for two cases of hydraulic fracturing induced seismicity in Ohio, inferred from the temporal correlation of either a maximum count of seismicity or the largest magnitude event reported during the fracking treatment (Friberg et al., 2014; Skoumal et al., 2015). A recent study on remote dynamic triggering in three sedimentary basins in Canada, where recent fluid injection is correlated with increasing seismicity, also suggests that susceptibility to triggering and the mechanism of instantaneous versus delayed triggering may be related to the relative influences from pore pressure and solid matrix stress changes (Wang et al., 2015). Future poroelastic stress modeling work using realistic injection history, formation permeability structure and fault orientation is needed to quantitatively verify the casual relation.

3.2 Maximum magnitude

One of the most critical issues of induced seismicity hazard assessment is whether there exists a magnitude-predictable relationship between operation parameters (i.e., total injection volume, volume rate, wellhead pressure, etc.) and induced events, and if yes how to develop such a relationship. While a fundamental step in the development of such a relationship relies on the understanding of the physical processes of induced earthquakes, first-order estimates on the maximum magnitude have been explored by several studies (e.g., McGarr, 2014; Dieterich et al., 2015; Ampuero et al., 2016). Each of these estimates involves a set of assumptions about the source processes, some of which appear plausible but are difficult to prove. For example, McGarr (2014) derived that the maximum moment of an induced earthquake is proportional to the total injection volume $M_0(\text{max})=G\Delta V$ (G is shear modulus, ΔV is injection volume), by assuming that (1) induced earthquakes have shear stress drops proportional to the pore pressure increase calculated from the injected fluid volume, (2) induced seismicity follows the Gutenberg-Richter magnitude-frequency distribution, and (3) the strain change within a defined volume is proportional to the cumulative

moment of all earthquakes in that volume (Kostrov, 1974). A similar scaling of $M_w \sim \log_{10}(V)$ is derived by Dieterich et al (2015) from a different line of reasoning, assuming that the volume of the pressurized crust V would be proportional to the injected volume ΔV at least during the initial injection period. Although the above relationship initially agrees with data from some wastewater disposal, fracking and enhanced geothermal wells, more recent studies clearly showed that some WCSB fracking induced earthquakes have seismic moments up to 100 times of the McGarr's upper limit prediction, despite their small to moderate total injection volumes compared to those in disposal wells (British Columbia Oil and Gas Commission, 2015; Atkinson et al., 2016). Another statistical study on induced seismicity in the US mid-continent also found the injection rate of a well, rather than its total injection volume or monthly wellhead pressure, is much more strongly associated with seismicity, and suggested that management of well injection rates could be a useful tool in reducing potential induced seismic hazard (Weingarten et al., 2015). Depending on the relative distances between the wells and receiver faults, stress perturbations from multiple wells can make cumulative contributions to promoting fault instability (Walsh and Zoback, 2016).

Alternatively, van der Elst et al. (2016) suggested that, while the total number of induced earthquakes may be related to the injection parameters, once the fluids permeate to a pre-existing fault and promote seismic slip on it, the maximum magnitude of such earthquakes should follow the Gutenberg-Richter magnitude-frequency distribution assuming no upper bound. The distinction between the two hypotheses for the maximum magnitude lies exactly on the induced earthquake source processes, in that the McGarr (2014) and Weingarten et al. (2015) model assumes events occur in the vicinity of the injection sources whereas the van der Elst et al. (2016) model assumes tectonics plays a more important role in controlling how large the earthquakes can potentially grow, although the nucleation may be due to fluid injection.

4. Public and regulatory policies

4.1 Impact of induced earthquakes on short-term seismic hazard maps

Ground motion prediction plays a crucial role in seismic hazard assessment and preparation. Consequently, it is intriguing to investigate whether induced earthquakes produce similar ground shaking as natural events do. Using spatially rich intensity data from the USGS "Did You Feel It" system, Hough (2014) suggested that induced earthquakes have lower effective intensity magnitude than natural earthquakes in the central and eastern US (CEUS), indicating that less ground shaking will be generated by induced earthquakes than tectonic

earthquakes, despite of shallower focal depths of the former.

Another intriguing yet critical question is how to incorporate the recent occurrences of induced seismicity into the national earthquake hazard map based on probabilistic analysis (Petersen et al., 2015). After considering the recent short-term (2014-15) seismicity rates and assuming the activity rate will remain stationary over next year, the updated one-year hazard map shows significant impact from the induced earthquakes in that hazard is 3- to 10-fold higher near some areas of active induced earthquakes than in the 2014 USGS National Seismic Hazard Model, which did not consider induced earthquakes (Petersen et al., 2016). A striking feature is that in the 2016 one-year model of Modified Mercalli Intensity (MMI) the 1% probability of exceedance in one year appears to be higher in Oklahoma than the long recognized New Madrid Seismic Zone in central US, highlighting the necessity of taking into account of induced earthquakes for seismic hazard assessment.

4.2 Traffic light protocols

Given the global increasing energy demand, anthropogenic processes that can induce earthquakes seem inevitable. A proper protocol of such anthropogenic processes is necessary to reduce the potential damage and property losses by the induced earthquakes. A “traffic light” system is a seismic hazard management plan that the industry and government regulators develop for their decision-making process in

response to the occurrence of earthquakes associated with anthropogenic activities.

Traffic light protocols (TLP) for induced seismicity was first proposed for regulations of hydraulic stimulations of geothermal systems (Bommer et al. 2006), where the peak ground velocity (PGV), induced earthquake magnitude, and seismicity rate are all considered in the determination of the “traffic lights”. For example, the TLP developed for the enhanced geothermal operations in Basel, Switzerland, consists of 4 levels, green, yellow, orange, and red, moving up the scale as the above criteria exceed certain preset thresholds and corresponding action plans by the industrial operators and government regulators (Håring et al., 2008). A green light is issued when $PGV < 0.5$ mm/s, local magnitude $M_L < 2.3$, and there are no felt reports. A yellow light is given when $PGV \leq 2.0$ mm/s, $M_L \geq 2.3$ and few felt reports. Operators need to inform regulators and stop increasing pumping rate. An orange light is given when $PGV \leq 5$ mm/s, $M_L \geq 2.9$ and many felt reports. In such a case, the operators must reduce wellhead pressure by decreasing pumping or by bleeding the well. When PGV exceeds 5 mm/s and local magnitude is greater than 2.9 with generally felt reports, pumping must stop and wells need to be kept at the minimum wellhead pressure (Håring et al., 2008). The criteria and cut-off thresholds used in TLP for different types of operations vary considerable in different regions and countries. Table 1 summarizes the TLPs currently in practice in Europe and North America (Kao et al., 2016).

Table 1 Summary of Traffic light protocols (TLP) currently in practice in Europe and North America^{a)}

Country/State/Province	PGV (mm/s)	M_L	Felt reports	TLP
Basel, Switzerland	< 0.5	< 2.3	No	Green
	≤ 2.0	≥ 2.3	Few	Yellow
	≤ 5.0	≥ 2.9	Many	Orange
	> 5.0	> 2.9	General area	Red
UK		≥ 0.0		Yellow
		≥ 0.5		Red
Colorado, US			Felt at surface	Yellow
		> 4.5		Red
Ohio, US	Buffer zones around high risk areas			Yellow
		≥ 1.0		Red
Oklahoma, US	Areas of interest (10 km from any $M4+$ events or $M3+$ swarms)			Yellow
		≥ 1.8 to 3.7^*		Red
Alberta, Canada		≥ 2.0		Yellow
		≥ 4.0		Red
British Columbia, Canada		≥ 4.0		Red

a) Modified from Kao et al. (2016). In general, a “yellow” light requires the operators to modify operation parameters (e.g., pumping rate, wellhead pressure). Operations must stop under a “red” light. *Exact TLP thresholds are determined on a well-to-well basis (Wong et al., 2015).

5. Discussion and perspective

5.1 Source properties and seismicity patterns of induced and natural earthquakes

Despite the recent progress on the induced earthquakes, it is still challenging to reliably discriminate injection-induced (anthropogenic) and natural (tectonic) earthquakes. The source parameter approach has been shown to be effective in making direct comparisons between individual events. In practice, earthquake source properties, focal mechanism and stress drop can provide insights to the faulting process that generated the seismic event.

While most tectonic earthquakes have nearly pure double-couple (DC) moment tensor solutions, some earthquakes related to fluids of either natural or anthropogenic causes are reported to have significant non-DC components due to complex local fracturing processes. For example, mixed non-double-couple and shear motions have been inferred for volcanic earthquakes (Julian et al., 1998) and events accompanied by rapid fluid flow during crack opening in geothermal fields (Guilhem et al., 2014). A recent study using full waveform inversion also found that eight $M_w \geq 3.5$ induced earthquakes in the WCSB have significant isotropic and CLVD components, with the 2015/06/13 $M_w 4.1$ Fox Creek event reaching a combined ISO and CLVD of 70% (i.e., only 30% DC component) (Zhang et al., 2016). Such large non-DC source mechanisms can arise from a variety of processes including the activation of multiple, sub-parallel shear fractures due to high pressure during injection, the creation of damage and rock porosity change caused elastic moduli variations, or combined effects of the above factors. However, we note that having a significant non-DC component in the moment tensor solution is not a sufficient condition for discriminating injection-induced versus tectonic events. Complex local fracturing process can result in large non-DC components for tectonic earthquakes such as in a volcanic system (Julian et al., 1998), meanwhile induced earthquakes on pre-existing faults may exhibit primarily DC focal mechanism (McNamara et al., 2015). For example, another $M_w 4.1$ Fox Creek event on 2016/01/12 was shown to have limited non-DC component (~22%) (Wang et al., 2017).

Static stress drop, the shear stress change on a fault before and after an earthquake, might shed light on the different source processes of induced and natural earthquakes. Hough (2014) suggested that the stress drop of induced earthquakes in CEUS may be lower than their tectonic counterparts, although this study used USGS ground shaking intensity distribution as a proxy for stress drop values. In contrast, two recent studies analyzing the spectra or spectra ratios of induced earthquakes in the WCSB have found that these events have stress drop values between 1 and 100 MPa (Zhang et al., 2016; Clerc et al., 2016), within the range and even

on the high end of typical tectonic earthquake stress drops (0.1–100 MPa). Stress drop estimates often have notoriously large uncertainties due to attenuation along the wave path, site responses, and the ambiguities in applying different spectra models to fit the corner frequencies. While influence of the first two factors may be alleviated with the empirical Green's function approach, the last factor persists and makes it challenging to compare the face values of stress drops from individual studies. Accurate estimates of stress drops of different types of induced earthquakes and appropriate comparison to tectonic earthquakes from the same geographic region are thus key to future research on the source properties of induced seismicity.

In addition to the efforts to discriminate induced and natural earthquakes from their source properties, seismicity pattern analysis has been used to investigate induced earthquakes. The first approach is to find the difference between natural and induced seismicity by using some summarizing statistics. For example, Bachmann et al. (2012) found that the b -value in the magnitude-frequency relation is correlated to pore-pressure: the b -value decreases from the co-injection period to the post-injection period as well as decreases with the distance to the injection points. Using clustering analysis, Zaliapin and Ben-Zion (2016) studied features of induced earthquakes in the Geysers geothermal field in northern California and TauTona gold mine in South Africa, and compared to seismicity from some regular tectonic zones. They found several distinguishing characteristics of induced seismicity, such as higher rate of background events, faster temporal decay of clusters, higher rate of repeating events, larger proportion of small clusters, and larger spatial separation from the initiating event and other events in a cluster. These conclusions need to be verified by further studies.

5.2 Statistical and physics-based seismicity models

Statistical analysis on short-term seismicity such as the Epidemic-Type Aftershock Sequence (ETAS) model (e.g. Ogata, 1988; Ogata, 1998; Zhuang et al., 2002; Ogata and Zhuang, 2006) have been widely used for modelling the short-term earthquake clustering behavior and producing daily forecasts (e.g., Zhuang, 2011). The theories and techniques related to the ETAS model have been utilized to study induced seismicity (e.g. Llenos and Michael, 2013; Llenos and Michael, 2016). Using the change-point detection technique proposed by Ogata (1988), Llenos and Michael (2013) found changes in the background seismicity rate and triggering parameters in both Oklahoma and Arkansas, and concluded that swarms that occurred following fluid injection differ from swarms triggered by natural processes. Such changes were also confirmed by Wang P et al. (2016) and Gupta and Baker (2015) by using approaches of Bayesian model comparison. By fitting ETAS model to seismicity data from the Basel EGS sites,

Switzerland, Bachmann et al (2011) have found that the background seismicity rate shows good correlation with the pumping history in each time window. Using similar methods, Eto et al. (2013) draw the same conclusion for induced seismicity in the Yanizu-Nishiyama hydrothermal field, Japan. One key point of such statistical approach is to robustly estimate the background seismicity rate, which can be obtained from different methods, such as specifying background rate (e.g. Imoto, 2001), stochastic reconstruction method (Hainzl and Ogata, 2005; Hainzl et al., 2016), and using Bayesian analysis with smoothness prior (e.g., Ogata et al., 2003; Kumazawa and Ogata, 2014). To date, the Bayesian analysis, which has been shown powerful in detecting the changes of seismicity patterns due to known or unknown causes in the study of natural earthquakes (e.g., Ogata et al., 2003) or volcano induced swarms (Kumazawa et al., 2016), has not yet been introduced in the study of fluid injection induced seismicity.

Furthermore, comprehensive system-level models that couple physics-based simulations of seismicity with reservoir simulations of fluid pressure changes can provide an experimental capability to investigate topics related to induced seismicity (Dieterich et al., 2015). Using an earthquake simulator based on rate-state friction including injection history that leads to pore pressure variation over time, Dieterich et al., (2015) find that the spatial-temporal patterns of simulated injection-induced seismicity are quite sensitive to pre-injection fault stresses. Moreover, continuing seismicity following shut-in of injection appears to be driven primarily by delayed nucleation and decays by the Omori aftershock law. Although the initial work was done on an extremely simple fault and injection system (Dieterich et al., 2015), it lays out the foundation to target specific cases by incorporating realistic injection history, reservoir and fault geometry, as well as hydraulic properties.

5.3 Near-field and *in situ* observations

While many of fluid injection induced earthquakes occur in regions of seismic quiescence prior to oil and gas operations, the relatively sparse seismographic network in such areas may play a role in the lack of full characterization of nearby natural earthquakes. Numerous examples have underscored the importance of good network coverage for elucidating high-resolution spatial-temporal evolution of seismicity. For instance, seismicity recorded by the sparse regional network near the Hutubi gas repository usually has large uncertainties in locations (Zhang et al., 2017). Without mapping out in high resolution the local seismicity near injection sites, it is extremely difficult to understand by what mechanisms the fluid injection may cause earthquakes. Another challenge is that usually a significant portion of seismicity is missing by seismic network due to signal-noise-ratio of waveforms. Such small magnitude events can be detected by advanced

event detection algorithms such as the matched filter technique (Yang et al., 2009).

Even though we can improve the seismic network coverage rapidly, it is not sufficient to elucidate the mechanism of how fluid may trigger fault slip without *in-situ* observations. One recent experiment in France, the step-rate injection method for fracture *in situ* properties (SIMFIP), is probably the only case where triggered fault slip is directly observed. In the SIMFIP experiment a preexisting fault cutting through a carbonate formation accessible for examination and instrumentation was selected, allowing the simultaneous measuring of fault-normal displacements, fault-parallel displacements, and fluid pressure after fluid injection (Guglielmi et al., 2015a, b; Cornet, 2016). The authors observe highly dilatant and slow aseismic slip associated with reduced dilatancy and micro-earthquakes. Most aseismic slip occurs within the fluid-pressurized zone and obeys a rate-strengthening friction law. Fluid injection primarily triggers aseismic slip in this experiment, with micro-earthquakes being an indirect effect mediated by aseismic creep. This poses another significant question on how the fluid injections may promote fault slip, aseismic or seismic.

To tackle such challenges not only demands more *in situ* observations, which may be conducted by drilling projects involving multidisciplinary approaches, but also demands better understanding of how fault zone properties may be altered by injected fluids and control fluid migration. A fault zone (FZ) usually includes a fault core and the surrounding damage zone with highly fractured materials (e.g. Chester et al., 1993). Whether the fault zone acts as a conduit, a barrier, or a conduit-barrier combined system for fluids is determined by the grain-scale permeability of the fault core and the hydraulic properties of the fracture network in the damage zone (Caine et al., 1996). It has been suggested to use the ratio between the damage zone width and the fault zone width (damage zone width + fault core width) to quantify the barrier-to-conduit permeability structure (Caine et al., 1996), providing a plausible way to estimate the permeability structure of faults near the fluid injection points. In general the seismically observed damage zone is much wider than the fault core (e.g. Yang, 2010, 2015), and thus the fluid flow properties of the fault damage zone primarily controls how the fluid injection may promote slip on the fault. Excluding exhumed faults or FZ drilling projects, the damage zone structure is mostly quantified by modeling fault zone related waves, such as trapped waves (e.g. Li et al., 1990) and FZ-reflected body waves (e.g. Yang and Zhu, 2010; Yang et al., 2011, 2014). Most recently discovered damage zones extend to a shallow depth, 2–5 km below the surface (e.g. Yang and Zhu, 2010; Yang, 2015) and may exhibit along-strike variations (e.g. Yang et al., 2014). The damage zones reflect past rupture behaviors, and could promote future earthquake rupture propagation (Weng et al., 2016). Although high-resolu-

tion imaging of fault zone structure has been well developed, monitoring how the fault zone evolves over time in the field is still one of challenges in earthquake physics (Yang, 2015). In addition to the growing dense array deployments, high-quality repeating active sources (Wang et al., 2012) may advance our ability to continuously monitor temporal changes of fault zones at depth and thus provide critical keys in understanding how fluid injection may induce earthquakes.

5.4 Collaboration between academia, industry and government

The issue of induced seismicity is politically and emotionally charged. There is a delicate balance between the positive economic impacts of resource development and the public's concerns about the potential environmental impact of the infrastructure buildup, environmental contamination, and induced seismicity. The acquiring and preserving of "social licenses" for drilling and injection requires transparent translation from independent scientific knowledge to regulatory policies and operation protocols. A collaborative relationship among academia, industry and government, is crucial.

Geological Survey of Canada (GSC) launched the Induced Seismicity Research (ISR) project in 2012 under the Environmental Geoscience Program. One of the mandates of ISR is to provide scientific information to all levels of government for making public policies in the development of unconventional oil and gas and protection of public safety and environment. GSC has organized workshops in 2015 and 2016 with attendees from industry, government and academia to facilitate direct dialogs and collaborations (Kao et al., 2016). Regional seismic network coverage has been increasingly densified in the past few years in northeast British Columbia and Alberta to expand monitoring capability of induced earthquakes, through the joint effort of the federal and provincial government. Local dense arrays focusing on specific injection wells are also installed, including some stations directly on company properties, as research project based temporary deployments. Permanent regional station data are open to the public and individual PI based local array data are typically open after certain embargo periods. In addition, industrial operators are encouraged to share part of their private station data with academic researchers under confidential research agreements. All the above channels for collaboration have stimulated the induced seismicity research in Canada in the recent years.

Similar types of dialogues have taken place in the United States, such as the induced seismicity workshop co-hosted by the U.S. Geological Survey (USGS) and Oklahoma Geological Survey in 2014, during which participants from academia, industry and government discussed research agenda for incorporating induced seismicity in the US National Seismic Hazard Model (NSHM) and essentially laid the groundwork for

the development of the 2016 USGS one-year, regional seismic hazard map (Petersen et al., 2015; Petersen et al., 2016). Numerous reports have been published as a result of close collaborations between academia, industry and government. For example, the US Environmental Protection Agency has published a report with the title "Minimizing and Managing Potential Impacts of Injection-Induced Seismicity from Class II Disposal Wells: Practical Approaches" in February 2015. This report has been peer reviewed by experts from both industry and academia.

Currently, data sharing is the major challenge in the collaboration. Researchers need access to a full range of data, especially injection parameters and near-field seismograms from the industry to understand induced seismicity. However, because such datasets include embedded proprietary details, the industry would need strong incentives to agree to share with academic researchers and government agencies. Finding a protocol that will allow data sharing but also protect industrial proprietary information will be the next step stone towards understanding induced seismicity. This requires close and frequent conversations between all the stakeholders, including industry, academia, government, and the general public. Recently, the Canadian Association of Petroleum Producers (CAPP) has formed the Induced Seismicity Task Group, with 12 companies participating. The group has a mandate to "engage in deep sharing of industry best practices in mitigation and management of induced seismicity risk from hydraulic fracturing." Looking to the future, we hope a proper framework of operating guidelines and procedures will result from close collaborations.

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